# An investigation of catalysts for the on board synthesis of $NH_3$ . A possible route to low temperature $NO_x$ reduction for lean-burn engines

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Platinum group metal catalysts have been investigated for the formation of  $NH_3$  from  $NO + H_2$  at low temperatures in the absence and presence of CO. Although CO inhibits the formation of  $NH_3$ , substantial amounts are still observed with a Pt catalyst. By combining Pt with a support (ceria–zirconia) that has low temperature  $NO_x$  storage characteristics it has been shown in transient experiments that  $NH_3$  can be formed and stored *in situ* under rich conditions, and may then be used to reduce  $NO_x$  under lean burn conditions.

KEY WORDS: platinum metal catalysts; NO<sub>x</sub> reduction; lean-burn; ammonia storage.

## 1. Introduction

The development of fuel efficient lean-burn gasoline engines has resulted in major new challenges for emission control systems that are now required to satisfy the current environmental legislation. The release of nitrogen oxides (NO + NO<sub>2</sub>, commonly referred to as "NO<sub>x</sub>") is a particular problem because the excess oxygen in the exhaust of a lean-burn engine precludes the use of conventional three-way catalyst technology. Direct NO. reduction under lean-burn conditions was first attempted by using the residual hydrocarbons (mainly propene) in the exhaust. Many hundreds of catalyst formulations were screened but none were acceptable. When this use of residual hydrocarbons proved unsuccessful, the direct addition of a hydrocarbon reductant (such as the gasoline itself) into the exhaust in front of the catalyst was tried. Although this provided substantially greater levels of NO<sub>x</sub> reduction in laboratory experiments the general consensus is that this is still not a technically viable approach. Consequently, for gasoline engines the socalled "Toyota concept" in which NO<sub>x</sub> is stored in the catalyst under lean conditions and the NO<sub>x</sub> trap is regenerated by a short period under rich conditions, has found favour [1]. In Europe, however, there is still an issue with NO<sub>x</sub> traps because they are poisoned by sulphur oxides [1-5], and European gasoline still contains too high a level of sulphur to allow these  $NO_x$  traps to be used for long periods of time.

In the case of diesel engines the  $NO_x$  removal problem is further constrained because the sulphur level, even in "low sulphur diesel", is still much higher than in

gasoline. Moreover, the temperature of the diesel exhaust is significantly lower than in the case of a gasoline engine. Consequently, the kinetics of  $NO_x$  trapping, which requires oxidation of NO to  $NO_2$  as a first step [6,7], and regeneration, which requires decomposition of barium nitrate species, are barely adequate. Indeed, in the case of small diesel engines fitted with turbochargers, the temperature of the exhaust under urban driving conditions can be well below 200 °C, which may be contrasted with the >500 °C typically found with gasoline engines.

For heavy duty diesel engines, there is a growing interest in using  $NH_3$  to reduce  $NO_x$ , with the  $NH_3$  being produced on board a vehicle by the hydrolysis of a urea solution [8]. This approach derives from well-established technology for stationary applications (*e.g.* large power stations) where it is known that by judicious choice of catalyst it is possible to get an acceptable rate of reduction of  $NO_x$  at low temperatures [9]. Furthermore, as compared with the NO/hydrocarbon reaction, there is much less tendency to produce nitrous oxide ( $N_2O$ ), itself a hazardous greenhouse gas, as a by-product of the  $NH_3/NO_x$  reaction. In the NO/hydrocarbon case, at temperatures below about 250 °C,  $N_2O$  is the major product [10].

Richter *et al.* [11] have proposed using a zeolite to trap ammonia gas that can then be used for  $NO_x$  reduction at low temperatures. However, using  $NH_3$  storage for mobile applications is not ideal because this still requires regular replenishment of the reservoir. Consequently, the possibility of generating  $NH_3$  *in situ* from the  $NO_x$  in the exhaust has been advocated [12]. In this paper we present some preliminary results on the formation of  $NH_3$  on Platinum Group Metal catalysts at low temperatures, and the subsequent attempt to use this  $NH_3$  to reduce  $NO_x$ .

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# 2. Experimental

Catalysts, nominal composition 1% by weight, were prepared by incipient wetness impregnation of the oxide support (SiO<sub>2</sub> or CeO<sub>2</sub>-ZrO<sub>2</sub>) using aqueous solutions of Pt(II) DNDA, palladium nitrate, or rhodium nitrate). The prepared catalysts were dried at 120 °C overnight and then calcined at 500 °C for 2 h.

The activity of the various catalysts for the reaction between NO and  $H_2$ , in the absence or presence of CO, were investigated using a flow microreactor with online analysis by mass spectrometry. 100 mg catalyst was prereduced in  $3\%H_2/\text{He}$  at  $400\,^{\circ}\text{C}$  for 2 h and then exposed to a reaction mixture of 1000 ppm NO, 1000 ppm  $H_2$  in a He flow of  $200\,\text{cm}^3\,\text{min}^{-1}$ , giving a gas hourly space velocity of  $120\,000\,\text{h}^{-1}$ . Results were obtained by analysis of reactants and products as the temperature of the catalyst bed was raised from ambient to  $450\,^{\circ}\text{C}$  at a ramp rate of  $5\,^{\circ}\text{C}\,\text{min}^{-1}$ . The effect of CO on the formation of NH<sub>3</sub> was investigated by adding CO at the levels of 200 or 1000 ppm.

To investigate the feasibility of producing NH<sub>3</sub>, which could then be captured by the catalyst for subsequent reduction of NO<sub>x</sub>, pulse experiments were conducted in which NO (500 ppm) and O<sub>2</sub> (5000 ppm) were passed over the 1%Pt/CeO<sub>2</sub>-ZrO<sub>2</sub> catalyst at 200 °C. The flow of O<sub>2</sub> was cut off temporarily every 5 min and replaced by H<sub>2</sub> (2000 ppm) for 30 s.

#### 3. Results and discussion

Figures 1–3 show the results of the NO/H<sub>2</sub> reaction with the silica-supported catalysts. With Pt/SiO<sub>2</sub>, NH<sub>3</sub> is first observed at relatively low temperatures ( $<100\,^{\circ}$ C). NH<sub>3</sub> is the major nitrogen-containing product from 120 to *ca.* 350 °C, and the concentration increases up to a maximum at around 200 °C. In the case of Pd/SiO<sub>2</sub>, NH<sub>3</sub> is only observed above 150 °C and reaches a plateau at *ca.* 320 °C where it remains

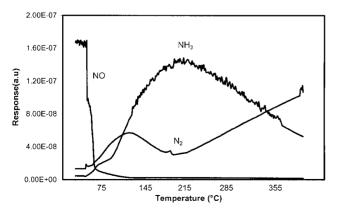


Figure 1.  $NO+H_2$  reaction over  $1\%Pt/SiO_2$ . (Reaction conditions: total gas flow:  $200\,ml/min$ ; catalyst weight:  $0.100\,g$ ; NO:  $1000\,ppm$ ;  $H_2$ :  $2000\,ppm$ ; He: balance).

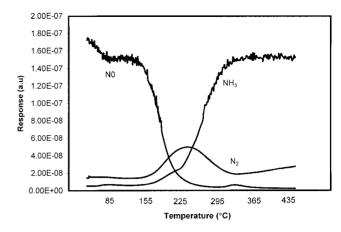


Figure 2.  $NO + H_2$  reaction over  $1\%Pd/SiO_2$ . (Reaction conditions: total gas flow: 200 ml/min; catalyst weight: 0.100 g; NO: 1000 ppm;  $H_2$ : 2000 ppm; He: balance).

the major nitrogen-containing product at all temperatures. The  $Rh/SiO_2$  catalyst produces the smallest amount of  $NH_3$  with formation first being observed at around 150 °C, followed by a flat maximum at ca. 270 °C before the concentration declines again.

Since the Pt/SiO<sub>2</sub> catalyst gives the highest concentration of NH<sub>3</sub> at the lowest temperature, the effect of CO was investigated. Figure 4 (compare also figure 1) shows that addition of CO has a significant effect on reducing the ability of the Pt to produce NH<sub>3</sub>. Thus, adding only 200 ppm CO raises the temperature at which NH<sub>3</sub> is detected from *ca.* 50 °C to about 125 °C, and adding 1000 ppm CO raises this temperature further to *ca.* 170 °C. However, even in the presence of CO, the formation of NH<sub>3</sub> is substantial.

To investigate whether any  $NH_3$  formed through the  $NO/H_2$  reaction could be trapped and used for subsequent reduction of  $NO_x$ , we selected a  $1\%Pt/CeO_2$ - $ZrO_2$  catalyst that in other work had been found to capture  $NO_x$  at low temperatures. Figure 5 shows that this material also produces substantial amounts of  $NH_3$  in the  $NO/H_2$  reaction at temperatures from

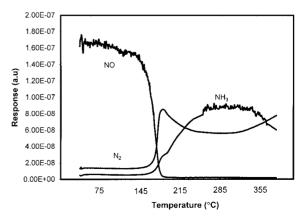


Figure 3.  $NO + H_2$  reaction over  $1\% Rh/SiO_2$ . (Reaction conditions: total gas flow:  $200 \, ml/min$ ; catalyst weight:  $0.100 \, g$ ; NO:  $1000 \, ppm$ ;  $H_2$ :  $2000 \, ppm$ ; He: balance).

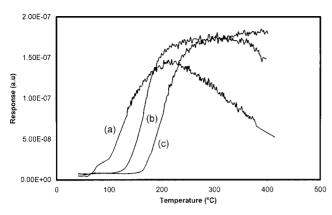


Figure 4.  $NO + H_2 + CO$  reaction over  $1\%Pt/SiO_2$ : effect of CO concentration. (Reaction conditions: total gas flow:  $200 \, ml/min$ ; catalyst weight:  $0.100 \, g$ ; NO:  $1000 \, ppm$ ;  $H_2$ :  $2000 \, ppm$ ; CO:  $200-1000 \, ppm$ ; He: balance). (a) no CO; (b) CO:  $200 \, ppm$ ; (b) CO:  $1000 \, ppm$ .

100 °C upwards with a broad peak at around 200 °C. Moreover, when CO (500 ppm) was added, figure 6 shows that although there is a drop in the production of NH<sub>3</sub> at lower temperatures, the formation at 200 °C is still substantial.

This 1%Pt/CeO<sub>2</sub>-ZrO<sub>2</sub> catalyst was selected, therefore, to test the concept that NH<sub>3</sub> could be formed under rich conditions from NO and H<sub>2</sub> and that this NH<sub>3</sub> could be used to react with NO<sub>x</sub> under lean conditions. Figure 7 shows the results of these pulse experiments. During the period when the O<sub>2</sub> is flowing, the NO concentration gradually increases but as soon as the O<sub>2</sub> is replaced by H<sub>2</sub> the NO concentration first increases, presumably due to desorption of NO<sub>x</sub> stored under lean conditions, and then decreases before slowly rising again during the lean period.

The most significant result, however, is the observation that the formation of  $N_2$  is observed for about 70 s even though the  $H_2$  is only present for 30 s. Thus, when the lean conditions are re-established,  $N_2$  is produced for about 40 s after the reductant is flushed from the system. Figure 7 shows that during this period the NO level

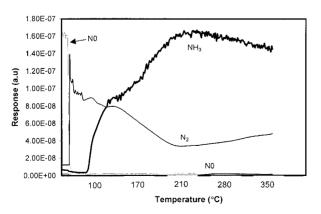


Figure 5. NO + H $_2$  reaction over 1%Pt/CeO $_2$ /ZrO $_2$  catalyst. (Reaction conditions: total gas flow: 200 ml/min; catalyst weight: 0.100 g; NO: 1000 ppm; H $_2$ : 2000 ppm; He: balance).

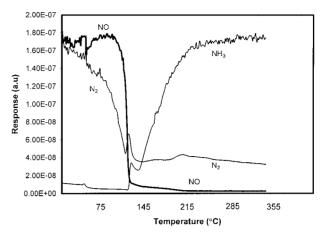


Figure 6.  $NO + H_2 + CO$  reaction over  $1\%Pt/CeO_2/ZrO_2$  catalyst. (Reaction conditions: total gas flow: 200 ml/min; catalyst weight: 0.100 g; NO: 1000 ppm;  $H_2$ : 2000 ppm; CO: 500 ppm; He: balance).

decreases while NH<sub>3</sub> is simultaneously observed. Since there is no way in which NH<sub>3</sub> could be produced from NO in the *absence* of H<sub>2</sub> we conclude that the NH<sub>3</sub> peak must arise from the formation of NH<sub>3</sub> while H<sub>2</sub> is present. Furthermore, the observation of an NH<sub>3</sub> desorption peak *after* removal of the H<sub>2</sub> suggests that the NH<sub>3</sub> has indeed been stored on the catalyst. Thus, it seems clear from these transient experiments that NH<sub>3</sub> can be formed *in situ*, trapped, and used to reduce NO<sub>x</sub>.

In summary, the formation of NH<sub>3</sub> from NO and H<sub>2</sub> at moderate temperatures has been demonstrated on Pt, Pd and Rh catalysts. In pulse experiments, it has been further shown that the outlet concentration of NO is

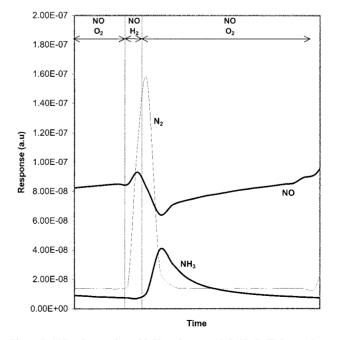


Figure 7. NO +  $O_2$  reaction with  $H_2$  pulse over  $1\%Pt/CeO_2/ZrO_2$  catalyst. (Reaction conditions: total gas flow:  $200 \, ml/min$ ; catalyst weight:  $0.100 \, g$ ; NO:  $500 \, ppm$ ;  $O_2$ : 0.5%;  $H_2$ :  $2000 \, ppm$ ; He: balance; reaction temperature:  $300 \, ^{\circ}C$ ).

lowered in transient experiments in which  $NH_3$  is observed. It is concluded that it would be possible, in principle, to use these catalysts to form  $NH_3$  in situ and then to use this  $NH_3$  to reduce  $NO_x$  at low temperatures under lean conditions.

## References

- N. Miyoshi, S. Matsumoto, K. Katoh, T. Tanaka, J. Harada, N. Takahashi, K. Yokota, M. Suguira and K. Kasahara, SAE Technical Paper 950809 (1995).
- [2] A. Amberntsson, B. Westerberg, P. Engstrom, E. Fridell and M. Skoglundh, Stud. Surf. Sci. Catal. 126 (1999) 317.
- [3] S. Matsumoto, Y. Ikeda, H. Suzuki, M. Ogai and N. Miyoshi, Appl. Catal. B 25 (2000) 115.

- [4] P. Engström, A. Amberntsson, M. Skoglundh, E. Fridell and G. Smelder, Appl. Catal. B 22 (1999) L241.
- [5] H. Mahzoul, L. Limousy, J. F. Brilhac and P. Gilot, J. Anal. Appl. Pyrol. 56 (2000) 179.
- [6] E. Fridell, H. Persson, B. Westerberg, L. Olsson and M. Skoglundh, Catal. Lett. 66 (2000) 71.
- [7] L. Olsson, B. Westerberg, H. Persson, E. Fridell, M. Skoglundh and B. Andersson, J. Phys. Chem. B 103 (1999) 10433.
- [8] W. Weisweiler, Chem. Ing. Tech. 72 (2000) 441.
- [9] A. Fritz and V. Pitchon, Appl. Catal. B 13 (1997) 1.
- [10] R. Burch and M.D. Coleman, Appl. Catal. B: Environmental 23 (1999) 115.
- [11] M. Richter, R. Eckelt, B. Parlitz and R. Fricke, Appl. Catal. B: Environmental 15 (1998) 129.
- [12] Y. Kinugasa, K. Igarashi, T. Itou, N. Suzuki, T. Yaegashi, T. Kanazawa, T. Hayashi, K. Yokota and Y. Nagai, US Patent 6,133,185 (17 October, 2000) to Toyota.